

## New concepts of microbial treatment processes for the nitrogen removal in wastewater

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### Abstract

Many countries strive to reduce the emissions of nitrogen compounds (ammonia, nitrate, NO<sub>x</sub>) to the surface waters and the atmosphere. Since mainstream domestic wastewater treatment systems are usually already overloaded with ammonia, a dedicated nitrogen removal from concentrated secondary or industrial wastewaters is often more cost-effective than the disposal of such wastes to domestic wastewater treatment. The cost-effectiveness of separate treatment has increased dramatically in the past few years, since several processes for the biological removal of ammonia from concentrated waste streams have become available. Here, we review those processes that make use of new concepts in microbiology: partial nitrification, nitrifier denitrification and anaerobic ammonia oxidation (the anammox process). These processes target the removal of ammonia from gases, and ammonium-bicarbonate from concentrated wastewaters (i.e. sludge liquor and landfill leachate). The review addresses the microbiology, its consequences for their application, the current status regarding application, and the future developments.

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**Keywords:** Nitrification; Anammox; Canon; SHARON; NO<sub>x</sub> cycle; Aerobic and anaerobic ammonia oxidation; Nitrogen removal; Wastewater treatment

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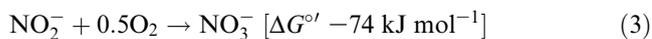
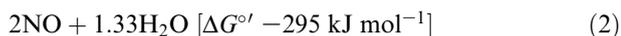
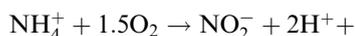
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## 1. Introduction

The three ammonium removal processes that are the focus of this review make use of (combinations of) three groups of chemolithoautotrophic bacteria: the well known ‘aerobic’ ammonia and nitrite oxidizers (Eqs. 1–3) and anaerobic ammonia oxidizers (Eq. 4). They all derive energy for microbial growth (CO<sub>2</sub> fixation) from the oxidation of inorganic nitrogen compounds:



For each of these three processes, microbiological aspects important for wastewater treatment are reviewed in the next sections.

## 2. Phylogeny and ecological niche

The evolutionary relationships (based on 16S rDNA phylogeny) of the chemolithoautotrophs of the nitrogen cycle are relevant to wastewater treatment, because 16S rDNA-based probing of populations of these organisms has been remarkably successful. Such 16S rDNA probes have been used to quantify the amounts of nitrifiers or anaerobic ammonia oxidizers in wastewater treatment plants [1–4]. In several cases probing resolved the mechanism of not-understood nitrogen conversions [5–7]. The probes were used to measure the in situ growth rates of relevant organisms in the actual plant [8,9]. The characterization of populations of nitrifiers using probes does not yet enable solid conclusions to improve plant management, but in view of the rapidly accumulating genomic data (<http://www.arb.de>), phylogenetic (16S) gene-probing may become part of the standard tools for daily plant management and optimization in the coming years.

### 2.1. Proteobacterial ammonia oxidizers

These ammonia oxidizing bacteria form two monophy-

letic groups, one within the beta- and one within the gamma-proteobacteria [3]. They are generally considered as aerobic chemolithoautotrophs, but recently organic compounds have been described that can serve them as carbon and energy source (see below). The beta-ammonia oxidizers comprise the well known genera *Nitrosomonas* and *Nitrospira* [10], *Nitrosococcus* is the gamma-proteobacterial genus [11], but does not include *Nitrosococcus mobilis*, that is related to *Nitrosomonas*. Different members of these genera have been found to dominate different wastewater treatment plants or natural ecosystems [2,4,8,12–17], but general relationships between the ecological niche and evolutionary position are often still obscure. The SHARON process (single reactor system for high-rate ammonium removal over nitrite; discussed below) is carried out largely by *Nitrosomonas europaea* [18]. The same bacterium is also one of the most capable denitrifiers (among nitrifiers) and was found to dominate the nitrifier denitrification (NO<sub>x</sub> process, see below). Salty wastewaters were found to be dominated by *N. mobilis* [2]. The genome project of *Nitrosomonas europaea* nears completion. Although the relevance of this organism for wastewater treatment is disputable, it will still provide an invaluable source of information.

### 2.2. Aerobic nitrite oxidizers

The second step of nitrification, the oxidation of nitrite to nitrate, is performed by nitrite oxidizing bacteria, e.g. members of the genera *Nitrobacter*, *Nitrococcus* and *Nitrospira* [19]. The first two genera are part of the alpha-proteobacteria, while *Nitrospira* is phylogenetically unrelated to any other cultivated species and forms a separate division [20].

Several strains of *Nitrobacter* and one strain of *Nitrospira* are the only nitrite oxidizers that are not restricted to marine environments [21,22]. There is some evidence that *Nitrospira* is the more specialized nitrite oxidizer. The other genera are more versatile, being facultative autotrophs and anaerobes, able to grow on heterotrophic substrates such as pyruvate and also capable of the first step of denitrification (the reduction of nitrate to nitrite) [21]. It appears that the genomes of nitrite oxidizers will not become available in the near future.

### 2.3. Anaerobic ammonia oxidizers

Anaerobic ammonia oxidation (anammox) is mediated

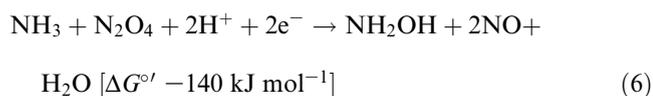
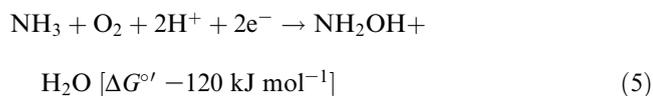
by a group of planctomycete bacteria [23], two of which have been named provisionally ('*Candidatus Brocadia anammoxidans*' [24] and '*Candidatus Kuenenia stuttgartiensis*' [6]). Retrieval of 16S rDNA sequences from anammox wastewater treatment has revealed several relatives of both species [7,25] and at least one other distinct group (Schmid et al., unpublished results). The molecular biodiversity of anammox bacteria is much larger than the diversity of their proteobacterial counterparts [26]. It is not yet known if or how the niche differentiation correlates with the phylogeny. This issue is important for application because the long start-up times of anammox reactors could be reduced significantly if it could be predicted how to seed a new reactor. The lack of pure cultures of anammox bacteria makes a genomic approach less straightforward in the near future.

### 3. Physiology

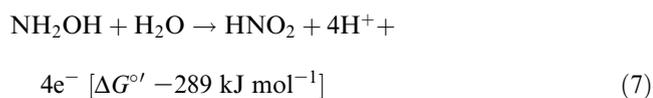
#### 3.1. Proteobacterial ammonia oxidizers

The physiology of conventional, 'aerobic' ammonia oxidizers is not completely understood. Only recently, it was discovered that these organisms also have an anaerobic metabolism (see below).

The proteobacterial ammonia oxidizers can obtain their energy for growth from both aerobic or anaerobic ammonia oxidation. Most likely ammonia ( $\text{NH}_3$ ) and not ammonium ( $\text{NH}_4^+$ ) is the substrate for the oxidation process [21]. The main products are nitrite under oxic conditions and dinitrogen, nitrite and nitric oxide under anoxic conditions [27,28]. Aerobic (Eq. 1) and anaerobic ammonia oxidation (Eq. 2) is initiated by the enzyme ammonia monooxygenase (AMO), that oxidizes ammonia to hydroxylamine. Oxygen and dinitrogen tetroxide (dimer of  $\text{NO}_2$ ) are the most likely electron acceptors for this enzyme [27–33] (Eqs. 4 and 5).



The hydroxylamine resulting from ammonia oxidation is further oxidized to nitrite (Eq. 7) by the hydroxylamine oxidoreductase (HAO) [34–36].



The four reducing equivalents derived from this reaction enter the AMO reaction (Eqs. 5 and 6), the  $\text{CO}_2$  assimilation, and the respiratory chain [37]. The reducing equiv-

alents are transferred to the terminal electron acceptors  $\text{O}_2$  (oxic conditions) or nitrite (anoxic conditions) [33,37]. The reduction of nitrite under anoxic conditions leads to the formation of  $\text{N}_2$  resulting in a N-loss of  $45 \pm 15\%$ . Under anoxic conditions the ammonia oxidation activity is relatively low ( $2.5 \text{ nmol NH}_3 (\text{g protein})^{-1} \text{ min}^{-1}$ ). The doubling time is about 30 days at best and the biomass yield is  $0.13 \pm 0.019 \text{ g dry weight (g NH}_3\text{-N)}^{-1}$ . The  $K_s$  value for the substrate ammonia is about  $20 \mu\text{M}$  at pH values between 6.7 and 8.3. These organisms are reversibly or irreversibly inhibited by various carbon compounds [38,39]. In contrast to aerobic ammonia oxidation [40], ammonia oxidation under anoxic conditions is not inhibited by acetylene [41].

In the presence of oxygen, the produced NO can be oxidized to  $\text{NO}_2$ . Therefore, only small amounts of NO are detectable in the gas phase of *N. eutropha* cell suspensions [42]. According to Eq. 2  $\text{N}_2\text{O}_4$  is the oxidizing agent also under oxic conditions [41]. Hydroxylamine and NO are produced as intermediates. While hydroxylamine is further oxidized to nitrite (Eq. 7), NO is (re)oxidized to  $\text{NO}_2$  ( $\text{N}_2\text{O}_4$ ) (Eq. 8).



Recently, a model was developed to explain the role of  $\text{NO}_x$  in the metabolism of the ammonia oxidizers [41].

Under oxic conditions ( $> 0.8 \text{ mg O}_2 \text{ l}^{-1}$ ) aerobic nitrifiers convert ammonia to nitrite (see above). At an oxygen concentration below  $0.8 \text{ mg O}_2 \text{ l}^{-1}$  they use small amounts of the produced nitrite as terminal electron acceptors producing NO,  $\text{N}_2\text{O}$ , and  $\text{N}_2$  [43]. In the absence of nitrogen oxides, up to 15% of the converted ammonia can be denitrified [44]. *N. eutropha* was shown to nitrify and simultaneously denitrify under fully oxic conditions in the presence of  $\text{NO}_2$  or NO. Interestingly, there is no fixed stoichiometry measurable between ammonia and  $\text{NO}_x$  (NO) consumption under oxic conditions. The ratio of ammonia to  $\text{NO}_x$  consumption range between 1000:1 and 5000:1. Obviously, nitrogen oxides have a regulatory function in the metabolism of nitrifiers under oxic conditions, stimulating the denitrification activity [45]. Influenced by nitrogen oxides, ammonia oxidizers convert ammonia to gaseous dinitrogen (about 60% of the converted ammonia) and nitrite (just about 40% of the converted ammonia) [42]. The specific aerobic ammonia oxidation activity is stimulated by  $\text{NO}_2$ , with values increasing from  $33 \mu\text{mol NH}_3 (\text{g protein})^{-1} \text{ min}^{-1}$  without  $\text{NO}_x$  addition to  $280 \mu\text{mol NH}_3 (\text{g protein})^{-1} \text{ min}^{-1}$  and a denitrification activity of  $150 \mu\text{mol NO}_2^- (\text{g protein})^{-1} \text{ min}^{-1}$  in the presence of 50 ppm  $\text{NO}_2$  [42]. The biomass yield and the affinity for ammonia remain unchanged. Control experiments with *N. europaea* and *Nitrosolobus multififormis* have yielded similar results. The reaction mechanism is the same, but the activities vary. Nitrogen oxides are toxic for many other microorganisms (nitrite oxidizers, heterotrophic bacteria) [46]. Reducing the cell number and the ac-

tivity of the nitrite oxidizers by adding  $\text{NO}_x$  [42] can be desirable in wastewater treatment, because the nitrite formed by the ammonia oxidizers is not further oxidized to nitrate (i.e. nitrite oxidizers). This is important since the nitrite is needed for the denitrification by the ammonia oxidizers.

### 3.2. Aerobic nitrite oxidizers

As mentioned above, nitrite oxidizers are often more versatile than ammonia oxidizers. When growing autotrophically with nitrite, the biomass yield is 0.036 g dry weight (g nitrite-N)<sup>-1</sup>, at a maximum growth rate of 0.04 h<sup>-1</sup> [47]. The apparent activation energy of nitrite oxidation is 44 kJ mol<sup>-1</sup> [48]. Like the ammonia oxidizers, these bacteria can have high substrate affinities (around < 70 μM for nitrite and < 25 μM for oxygen). It has been reported that hydroxylamine, ammonia and NO can inhibit nitrite oxidizers [49], but a mechanism for such inhibitions has not yet been proposed.

The key enzyme of nitrite oxidizing bacteria is the membrane-bound nitrite oxidoreductase [50] which oxidizes nitrite with water as the source of oxygen to form nitrate [51]. The electrons released from this reaction are transferred via a- and c-type cytochromes to a cytochrome oxidase of the aa<sub>3</sub>-type. However, the mechanism of energy conservation in nitrite oxidizers is still unclear. Neither Hollocher et al. [52] nor Sone et al. [53] was able to find any electron transport chain-linked proton translocation, which is necessary to maintain a proton motive force for ATP regeneration. Thus, NADH is thought to be produced as the first step of energy conservation [49]. Nitrite oxidizers are generally lithoautotrophic organisms [54]. Higher growth rates are obtained when the cells are growing mixotrophically [55,56]. Several strains of *Nitrobacter* are capable of heterotrophic growth under oxic as well as anoxic conditions [57,58]. Heterotrophic growth is significantly slower than lithoautotrophic growth [57], although 10–50-fold higher cell densities are obtained [21]. Some strains of *Nitrobacter* were shown to be denitrifying organisms as well. Under anoxic conditions, nitrate can be used as an acceptor for electrons derived from organic compounds to promote anoxic growth [59]. Since the oxidation of nitrite is a reversible process, the nitrite oxidoreductase can reduce nitrate to nitrite in the absence of oxygen [60]. Nitrite oxidation occurs obligatory under oxic conditions. The involved organisms are much more sensitive to oxygen limitation than ammonia oxidizers are. Already at dissolved oxygen concentrations of about 0.5 mg l<sup>-1</sup> nitrite oxidation is completely inhibited [61]. Additionally, *Nitrobacter* is inhibited at high oxygen concentrations [62]. Thus, the oxygen content of a nitrite oxidizing nitrification vessel has to be maintained carefully to avoid accumulation of nitrite. With sufficient oxygen supply nitrite oxidation proceeds at a faster rate than conversion of ammonia to nitrite. Therefore, high nitrite concentrations

are rarely found neither in natural environments nor in wastewater treatment plants [21].

### 3.3. Anammox

The physiology of the anaerobic ammonia oxidizer '*Candidatus Brocadia anammoxidans*' has been studied in detail. The bacterium is a chemolithoautotroph, has a doubling time of 11 days and the biomass yield is 0.13 g dry weight (g NH<sub>3</sub>-N)<sup>-1</sup> [63]. It has a very high affinity for the substrates ammonia and nitrite [64]. It is reversibly inhibited by oxygen and irreversibly by nitrite (at concentrations in excess of 70 mg N l<sup>-1</sup> for several days) and phosphate (> 60 mg P l<sup>-1</sup> for several days) [64–66]. The apparent activation energy is approximately the same as for aerobic ammonia oxidation: 70 kJ (mol NH<sub>3</sub>)<sup>-1</sup> [64]. '*Candidatus Kuenenia stuttgartiensis*' has a higher, but still low, tolerance to nitrite (180 mg N l<sup>-1</sup>) and phosphate (600 mg P l<sup>-1</sup>) [7]. Both bacteria have a similar temperature (37°C) and pH (8) optima.

Anammox bacteria do not consume ammonia and nitrite in a ratio of 1:1, as might be expected from their catabolism (Eq. 4), but in a ratio of 1:1.3. The excess nitrite (0.3 mol of nitrite per mol of ammonia) is oxidized anaerobically to nitrate. The electrons derived from this oxidation are probably used for the fixation of CO<sub>2</sub> [66].

The biochemistry of the anammox bacteria is not yet completely resolved. It is known that the anaerobic oxidation of ammonia proceeds via hydrazine (N<sub>2</sub>H<sub>4</sub>), a volatile and toxic intermediate [67,68]. An enzyme that resembles HAO from aerobic ammonia oxidizers is responsible for the oxidation of hydrazine to dinitrogen gas ( $\Delta G^{\circ} = -288$  kJ mol<sup>-1</sup>) [69]. It has been postulated that the electrons from this oxidation are channelled to nitrite leading to the production of hydroxylamine ( $\Delta G^{\circ} = -22.5$  kJ mol<sup>-1</sup>). Hydroxylamine and ammonia could yield hydrazine in a condensation reaction ( $\Delta G^{\circ} = -46$  kJ mol<sup>-1</sup>), which completes the catalytic cycle.

The ultrastructure of *B. anammoxidans* has many features in common with previously described planctomycetes (Fig. 1). These microorganisms have a proteinaceous cell wall lacking peptidoglycan and are thus insensitive to ampicillin. Anammox catabolism is at least partly located in a membrane-bound intracytoplasmic compartment, known as the anammoxosome [69]. All anammox cells have exactly one anammoxosome [69]. Anammoxosomes can be isolated intact from anammox cells [70]. They contain little or no RNA or DNA [69] and are surrounded by a dedicated membrane that is very impermeable because it consists of ladderane lipids [70]. The bacterial nucleoid is located on the outside of the anammoxosome membrane; it is extremely condensed as is the case for the other planctomycetes. Fig. 1 shows the ultrastructure of the anammox bacterium '*Candidatus Brocadia anammoxidans*'. Interestingly, *B. anammoxidans* [70] as well as aerobic ammonia

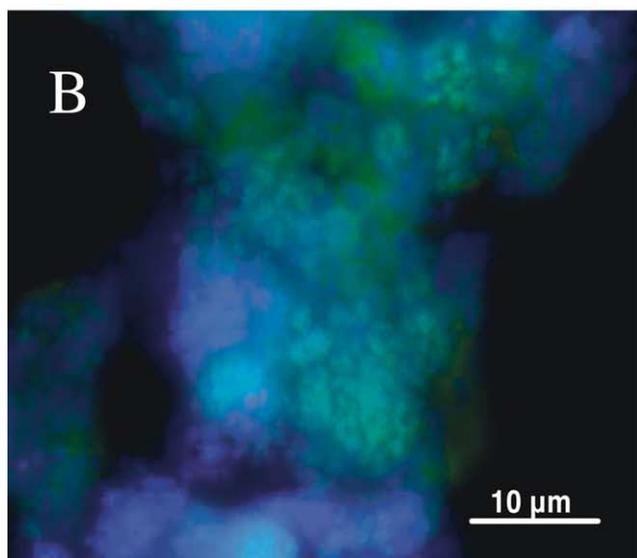
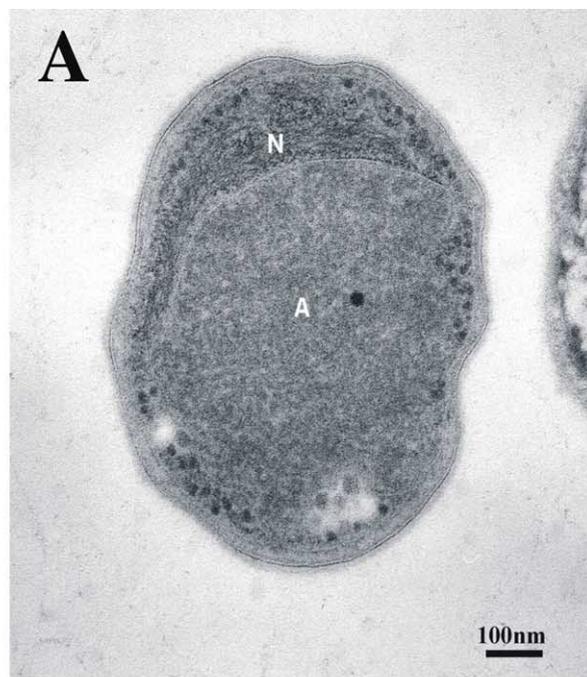


Fig. 1. A: Ultrastructure of the anammox bacterium *Candidatus* 'Brocadia anammoxidans'. A, anammoxosome; N, bacterial nucleoid. Bar: 100 nm. B: Two different anammox microorganisms in a mixed population. Green: *Candidatus* 'Kuenenia stuttgartiensis' and, Blue: *Candidatus* 'Brocadia anammoxidans Dokhaven 1'.

oxidizers like *Nitrosomonas* develop internal membrane systems.

### 3.4. Heterotrophic nitrification

The oxidation of ammonia [71], hydroxylamine [72] or organic nitrogen compounds, e.g. oximes [73], to nitrite and nitrate by various chemoorganotrophic microorganisms is called heterotrophic nitrification. The latter is a cometabolism which is not coupled to energy conservation [74]. Heterotrophic nitrifiers are found among algae [75],

fungi [76] and bacteria [77]. Compared to those of autotrophic nitrifiers nitrification rates of heterotrophic nitrifiers are low [78]. Therefore, heterotrophic nitrification was thought to occur preferentially under conditions which are not favorable for autotrophic nitrification, e.g. acidic environments [79].

### 3.5. Denitrification

Denitrification is the reduction of oxidized nitrogen compounds like nitrite or nitrate to gaseous nitrogen compounds. This process is performed by various chemoorganotrophic, lithoautotrophic, and phototrophic bacteria and some fungi [80,81], especially under oxygen-reduced or anoxic conditions [82]. Denitrification can be described as a kind of anoxic respiration. Electrons originated from e.g. organic matter, reduced sulfur compounds, or molecular hydrogen are transferred to oxidized nitrogen compounds instead of oxygen in order to build up a proton motive force usable for ATP regeneration. Enzymes involved are the nitrate reductase, the nitrite reductase, the nitric oxide reductase, and finally the nitrous oxide reductase [83,84]. Dinitrogen is the main end product of denitrification while the nitrogenous gases (nitric oxide and nitrous oxide) are occurring as intermediates in low concentrations [85]. However, these gases are also released as end products when denitrification enzymes are not completely expressed, e.g. when the concentration of dissolved oxygen is too high [86]. Denitrification also occurs in the presence of oxygen. The range of oxygen concentrations permitting aerobic denitrification is broad and differs from one organism to another [77]. The onset of aerobic denitrification is not depending on oxygen sensitivity of the corresponding enzymes, but rather on regulation of oxygen- or redox-sensing factors involved in the regulation on a transcriptional level.

## 4. Processes for N-removal

The newly discovered anaerobic ammonia oxidizing planctomycetes and the anaerobic metabolism of proteobacterial ammonia oxidizers open up new possibilities for nitrogen removal from wastewater. More specifically, the paradigm that the only way to biologically convert wastewater ammonium to dinitrogen gas necessitates the complete oxidation to nitrate followed by heterotrophic denitrification, has become obsolete. In this section the application of the new microbial possibilities is discussed.

### 4.1. Partial nitrification

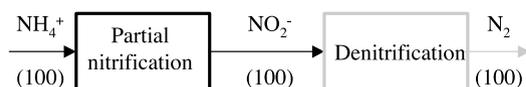
Partial nitrification is the oxidation of wastewater ammonium to nitrite (Eq. 1, Fig. 2), but not to nitrate. To achieve partial nitrification, the subsequent oxidation of nitrite to nitrate must be prevented. Partial nitrification

can be combined with the anammox process (see below), but even if it is combined with conventional denitrification (the so called ‘nitrite route’), already a significant benefit is achieved in terms of use of resources [48]. The process needs less aeration, the subsequent denitrification consumes less COD (chemical oxygen demand), since only nitrite and not nitrate has to be reduced to molecular nitrogen ( $N_2$ ). This is cost-effective if the low C/N ratio of the wastewater necessitates the addition of a synthetic electron donor, such as methanol. In that case the process also emits less  $CO_2$  to the atmosphere.

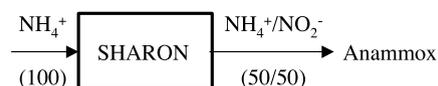
The oxidation of nitrite to nitrate can be prevented in at least two ways. First, by making use of the difference in activation energy between ammonia and nitrite oxidation ( $68 \text{ kJ mol}^{-1}$  and  $44 \text{ kJ mol}^{-1}$ , respectively). The high activation energy of ammonia oxidation makes the rate of this process more dependent on temperature. The SHARON process (Fig. 2) makes use of the different growth rates of ammonia and nitrite oxidizers at sufficiently high temperatures (more than  $26^\circ\text{C}$ ) [48,87]. It works at a hydraulic retention time higher than the growth rate of nitrite oxidizers but lower than ammonia oxidizers (about 1 day). Because this process has no sludge retention nitrite oxidizers are not able to remain in the SHARON reactor and they are washed out. Because SHARON depends on high temperature, it is not suitable for all wastewaters (but many wastewaters high in ammonium also have a high temperature, such as sludge liquor). Furthermore, because there is no sludge retention and the hydraulic retention time is fixed, the volumetric ammonium reactor loading depends on the ammonium concentration. Thus, the process costs also depend on the ammonium concentration (rising costs with decreasing ammonium concentration). Aeration is not only necessary for oxygen supply, but also to strip  $CO_2$  from the reactor to control the pH. SHARON still makes use of denitrification (with added methanol) to reduce the nitrite to dinitrogen gas. Methanol is supplied periodically while the aeration is switched off. The stripping of  $CO_2$  combined with the addition of methanol neutralizes all the protons formed in Eq. 1 – if bicarbonate is the counter-ion for the wastewater ammonium. SHARON has been scaled-up and applied successfully at the Rotterdam wastewater treatment plant, for the treatment of sludge liquor. The  $1500\text{-m}^3$  reactor is in operation for 2 years and treats  $1000 \text{ kg N day}^{-1}$  [88].

A variation on the SHARON process does make use of sludge retention. Instead of the hydraulic retention time, here the sludge age is controlled (in SHARON, the hydraulic retention time equals the sludge age) [89]. This allows higher ammonium loading rates and more efficient aeration. The process also makes use of a second principle to prevent nitrite oxidation; at low oxygen concentrations (less than  $0.4 \text{ mg l}^{-1}$  or 5% air saturation) and with surplus ammonium, nitrite oxidizers are unable to grow, and nitrite becomes the stable end product of nitrification. It is unclear why nitrite oxidizers are inhibited; inhibition of

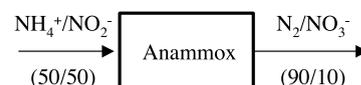
### 1a. Partial nitrification



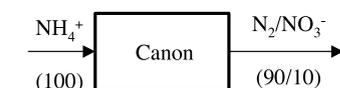
### 1b. Partial nitrification (SHARON)



### 2. Anammox



### 3. Canon



### 4. NOx-process

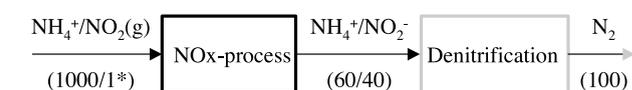


Fig. 2. Flux diagrams of the partial nitrification (1a.), SHARON (1b.), anammox (2.), Canon (3.), and  $NO_x$  process (4.). (< number > N-compound in % (values idealized; they may vary depending on process parameter), (g) gaseous  $NO_2$  (nitrogen dioxide). \*In the presence of oxygen the supplemented  $NO_2$  acts as regulatory signal (not as a substrate), inducing the denitrification activity of the aerobic ammonia oxidizers.

nitrite oxidizers by ammonia and a lower affinity for oxygen and/or nitrite have been suggested as possible explanations, but we still lack mechanistic evidence. This process has not yet been applied at full scale.

### 4.2. Anammox

The anammox process (Fig. 2) is the denitrification of nitrite with ammonia as the electron donor [90,91]. Anammox needs a preceding partial nitrification step, that converts half of the wastewater ammonium to nitrite. A modified SHARON process has been applied successfully in the laboratory to generate such ammonium/nitrite mixtures [91,92]. By simply not supplying any methanol and removing the anoxic periods, a SHARON reactor yields the desired ammonium/nitrite mixture, without the need for feedback control. This is possible because after 50% of the ammonium is oxidized, the decrease in pH (to 6.7) prevents the oxidation of the remaining ammonium. By limiting the oxygen supply to a nitrification reactor with

sludge retention, the same result can be obtained, although feedback control might be necessary [89].

The first full-scale anammox reactor is currently being built in Rotterdam, The Netherlands, as an addition to the SHARON reactor that is already in place. The reactor is estimated to have a return on investment of less than 7 years, because addition of methanol (currently used to sustain the denitrification) will no longer be required.

Laboratory experiments and design calculations have shown that anammox reactors will be extremely compact with volumetric ammonium loading rates of more than 15 kg N m<sup>-3</sup> day<sup>-1</sup>. Depending on the ammonium concentration of the wastewater and the reactor design, the dinitrogen gas produced by the process could at least partially mix the reactor (analogous to upflow anaerobic sludge blanket process (UASB) reactors), leading to very low power consumption. Additional mixing could be provided by recycling part of the produced dinitrogen gas. Due to the low growth rate of the responsible bacteria, sludge retention is extremely important. The reactor should be well mixed (to keep the redox potential in the ‘denitrification zone’ and prevent formation of toxic sulfide) and should not be overloaded, because high nitrite concentrations (more than 70 mg N l<sup>-1</sup> NO<sub>2</sub><sup>-</sup> ‘*Candidatus* Brocadia anammoxidans’, more than 180 mg N l<sup>-1</sup> NO<sub>2</sub><sup>-</sup> ‘*Candidatus* Kuenenia stuttgartiensis’) for extended periods are also detrimental to the process [64,66].

On laboratory scale, anammox has been tested in different reactors: fixed bed [89], fluidized bed [66], sequencing batch [63], and gas-lift reactors (unpublished results) all appeared to be suitable, although the economics of the process differ for the different reactor configurations (depending on existing reactors already in place that could be adapted to the process). One of the main challenges of the anammox process is the long start-up time. Because the anammox planctomycetes grow so slowly (see above) it takes between 100 and 150 days before an anammox reactor inoculated with activated sludge reaches full capacity [92]. Experience in anaerobic wastewater treatment (with UASB reactors) has shown that this problem may be overcome once the first full-scale anammox plants are in operation and seeding will become possible.

#### 4.3. Canon

Canon is an acronym for ‘completely autotrophic nitrogen removal over nitrite’. This concept (Fig. 2) is the combination of partial nitrification and anammox in a single, aerated reactor [89,93,94]. The name ‘Canon’ also refers to the way the two groups of bacteria cooperate: they perform two sequential reactions (Eqs. 1 and 4) simultaneously. The nitrifiers oxidize ammonia to nitrite, consume oxygen and so create anoxic conditions the anammox process needs. Canon has been tested extensively on laboratory scale. The volumetric loading rate (1.5 kg N m<sup>-3</sup> day<sup>-1</sup> in a gas-lift reactor) [94] is lower

than for anammox and also somewhat lower than has been achieved with high-end dedicated nitrification reactors. However, because only one reactor is required, the economics might still be advantageous when the daily ammonium load is low. Canon would need process control, to prevent nitrite build-up by oxygen excess.

The Canon concept has not been purposefully tested on pilot or full scale, but is known to occur accidentally in sub-optimally functioning full-scale nitrification systems [25,95–97]. Such systems combine three processes (Eqs. 1, 3 and 4), and convert ammonium to mixtures of nitrate and dinitrogen gas. The stoichiometry of the released products is influenced by e.g. the bacterial population and the physical parameters.

#### 4.4. NO<sub>x</sub> process

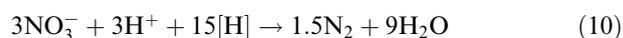
Controlling and stimulating the denitrification activity of *Nitrosomonas*-like microorganisms by adding nitrogen oxides offers new possibilities in wastewater treatment [98]. In the presence of NO<sub>x</sub> *Nitrosomonas*-like microorganisms nitrify and denitrify simultaneously even under fully oxic conditions with N<sub>2</sub> as main product (Fig. 2). Just about 40% of the ammonia load is converted to nitrite. Besides a 50% lower oxygen demand in the nitrification step (since nitrite is used as terminal electron acceptor), the subsequent denitrification step consumes less COD. The N-conversion in a combined nitrification/denitrification without NO<sub>x</sub> supply is shown in Eqs. 9–11 and N-conversions influenced by nitrogen oxides in Eqs. 12–14. The [H] represents the reducing equivalents (e.g. supplied by an external C-source). These results might vary depending on the composition of the wastewater.

Conventional plant

Nitrification



Denitrification

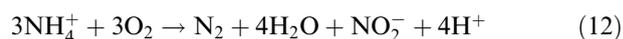


Sum

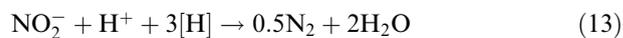


Plant with NO<sub>x</sub> supply

Nitrification



Denitrification



Sum



$\text{NO}_x$  ( $\text{NO}/\text{NO}_2$ ) is the regulatory signal inducing the denitrification activity of the ammonia oxidizers and it is only added in trace amounts ( $\text{NH}_4^+/\text{NO}_2$  ratio about 1000/1 to 5000/1) [45]. As a consequence about 50% of the reducing equivalents [H] are now transferred to nitrite as terminal electron acceptor (Eq. 12) instead of oxygen. Therefore the oxygen consumption of the process is reduced (Eqs. 12 and 14).

The new method for N-removal was developed in a laboratory scale reactor system allowing a performance increase as well as a decrease of the operating costs. The new process offers the possibility to be integrated into existing wastewater treatment plants with minimal financial and technical efforts.

One 2-m<sup>3</sup> pilot plant for the treatment of wastewater from intensive fish farming and a pilot plant of the company Nitra GmbH (Germany) at a municipal wastewater treatment plant (sludge liquor) were tested [99]. We will present data of a 3.5-m<sup>3</sup> plant. The installation is working for 22 months, treating highly loaded wastewater. Exhaust fume containing ammonia is processed via a washer and the effluent is treated in a nitrification/denitrification system equipped with the  $\text{NO}_x$  method. The highly loaded wastewater (about 2 kg  $\text{NH}_4^+-\text{N m}^{-3}$ ) is fed into the nitrification reactor (3 m<sup>3</sup>), which is connected to a stirred but not aerated denitrification tank (0.5 m<sup>3</sup>). The contact between the sewage and biomass is mediated via membrane surfaces (cross-flow filtration). The nitrification step is aerated with about 65 l air min<sup>-1</sup> supplied with 200 ppm  $\text{NO}_2$ .

The performance data of the nitrification step (without denitrification step) are presented in Fig. 3. The volume load of the plant was increased from about 2 kg  $\text{NH}_4^+-\text{N m}^{-3} \text{ day}^{-1}$  to about 4.7 kg  $\text{NH}_4^+-\text{N m}^{-3} \text{ day}^{-1}$ . The denitrification activity of the nitrifying biomass was very sensitive towards the  $\text{NO}_2$  supply. When the  $\text{NO}_2$  supply in the nitrification step was turned off between days 100 and 112, this led on short-term to an increased ammonia concentration caused by a reduced ammonia oxidation activity. The long-term effect was more interesting: a significantly increased nitrite concentration was detectable between days 112 and 150. Obviously, the denitrification activity of the ammonia oxidizers decreased when  $\text{NO}_2$  was not present (days 100–112). Under the influence of  $\text{NO}_2$ , the ammonia oxidizers again increased their denitrification activity (days 112–150).

During the 22-month operation time, the ammonia consumption in the nitrification step was about 3.5 times higher than the nitrite production. Since hardly any nitrate ( $< 1 \text{ g NO}_3^--\text{N m}^{-3}$ ) was formed and  $\text{NO}$  and  $\text{N}_2\text{O}$  were only detectable in small amounts (in waste gas  $< 40 \text{ ppm}$ ), strong evidence is given that the  $\text{N}_2$  production by ammonia oxidizers is mainly responsible for the average N-loss of about 67% (Fig. 4). Control tests under laboratory conditions confirmed these results [28,42]. The remaining N-load (nitrite) was removed in the small denitrification

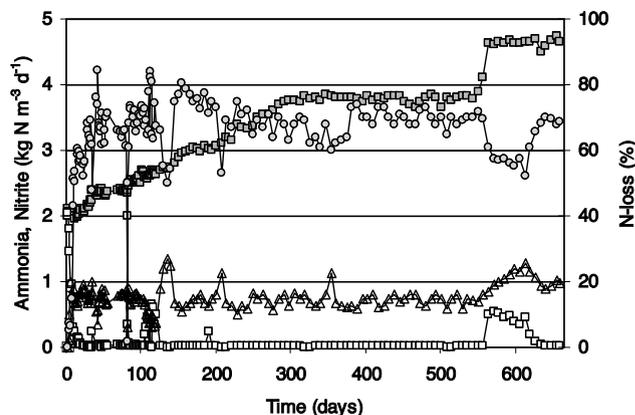


Fig. 3. Nitrogen balance of the  $\text{NO}_x$  process. Ammonia in (■), ammonia out (□), nitrite out (△), N-loss in the nitrification step (●). The N-loss is defined as the rate of soluble N-compounds converted into gaseous N-compounds (mainly  $\text{N}_2$ ).

step with methanol as carbon source. Including the denitrification step into the analysis of the nitrogen balance of the treatment plant, the N-loss was about 97% (Fig. 4). The costs to equip an existing sewage plant with a system for the  $\text{NO}_x$  supply were calculated with EUR 10 000–55 000 depending on the dimension of the plant. The method causes additional operating costs of EUR 0.05–0.08 per kilogram ammonia-N ( $\text{NO}_2$  supply). The following savings have to be taken into account: the external C-source can be reduced up to 80%, and the supply of oxygen can be reduced up to 50%.

#### 4.5. Further application

The OLAND process (oxygen-limited nitrification and denitrification) is described as a new process for one-step ammonium removal without addition of COD [100]. Apart from the basic fact that nitrifiers are involved, the mechanism is not yet understood and the ammonium loading rates are low. It seems possible that OLAND will be based on either the Canon concept (a combination

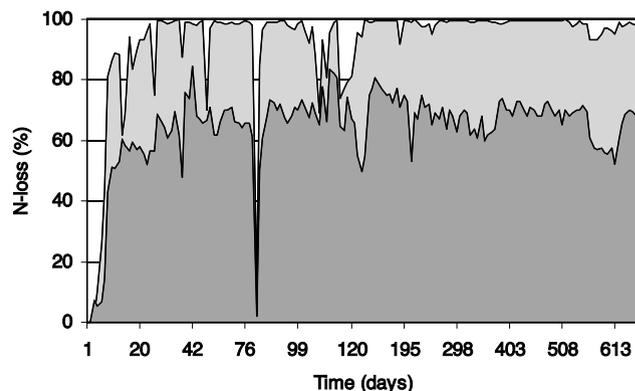


Fig. 4. N-losses in the nitrification step ( $\text{NO}_x$  process) and denitrification step; dark gray: nitrification step, gray: denitrification step.

Table 1  
Operational characteristics of wastewater treatment processes for nitrogen removal

	Conventional nitrification denitrification	NO <sub>x</sub>	OLAND	SHARON	Anammox	Canon	Aerobic deammonification
Aerobic ammonia oxidizers	many	<i>N. eutropha</i>	unknown	<i>N. eutropha</i>	absent	<i>N. eutropha</i>	unknown salt tolerant ammonia oxidizer
Aerobic nitrite oxidizers	many	absent	unknown	absent	absent	absent	<i>Nitrobacter</i>
Anaerobic ammonia oxidizers	absent	absent	unknown	absent	<i>B. anammoxidans</i> , <i>K. stuttgartiensis</i>	<i>B. anammoxidans</i> , <i>K. stuttgartiensis</i>	<i>K. stuttgartiensis</i>
Biofilms or suspension	biofilms/suspension	suspension	biofilms	suspension	biofilms	biofilms	biofilms
NH <sub>4</sub> <sup>+</sup> loading (kg N m <sup>-3</sup> reactor day <sup>-1</sup> )	2–8	5	0.1	0.5–1.5	10–20	2–3	1–2
N-removal efficiency	95%	95%	85%	90%	90%	90%	60%
Process complexity	separate oxic and anoxic compartments or periods, methanol dosing	separated oxic and anoxic compartments, methanol dosing, membrane for sludge retention	aeration needs to be tuned to ammonia loading	separate oxic and anoxic compartments or periods, methanol dosing	preceding partial nitrification needed	aeration needs to be tuned to ammonia loading	aeration needs to be tuned to ammonia loading
Application status	established	pilot plant	laboratory	two full-scale plants	full scale initiated	laboratory	two full-scale plants
Investment costs	medium	medium	medium	medium	low	medium	medium
Operational costs	high	low	unknown	low	very low	low	low

of aerobic and anaerobic ammonia oxidizers) or the NO<sub>x</sub> process (nitrifier denitrification in the presence of NO<sub>x</sub>).

The 'aerobic deammonification' process is another one-step ammonium removal process that does not depend on COD [25]. It has been tested on pilot plant and full scale, and converts part of the ammonium to dinitrogen gas and part to nitrate. Recently, it was discovered that this process is based on the Canon concept, with nitrifiers and anaerobic ammonia oxidizers cooperating under oxygen limitation. Because the 'aerobic deammonification' process evolved in reactors designed for conventional nitrification, the process design (a rotating biological contactor) is not optimal and the nitrogen loading rates and removal efficiency are low (Table 1).

## 5. Conclusion

Over the past 25 years, a significant amount of resources have been invested to construct wastewater treatment plants. Unfortunately, the performance of many of these facilities has not fulfilled the requirements of the discharge permits. In many cases, newly constructed plants have had to be retrofitted or modified at considerable expense to meet the discharge requirements and to provide more reliable performance. The need to conserve energy and resources is well documented, and therefore more attention is being paid to the selection of processes that conserve energy and resources. Operation and maintenance costs plus reliable process control are extremely important to operating agencies. Thus, the operability of treatment plants is receiving more attention. To design and operate a wastewater treatment system (activated sludge system) efficiently, it is necessary to understand the biochemistry of the involved microorganisms and basic research is the keystone to optimize established processes and to invent new and innovative systems. Discovering the group of anammox microorganisms opened new ways in nitrogen removal. Processes like SHARON and Canon have been developed, meeting the needs of treatment plants to handle e.g. high nitrogen-loaded wastewater. Also the discovery of the versatility of aerobic ammonia oxidizers led to the development of new treatment processes (e.g. NO<sub>x</sub> process). In the future the combination of the different groups of nitrogen converting microorganisms and the optimization of the process management (adaptation according to the wastewater composition; design of the treatment plants, temperature, oxygen and NO<sub>x</sub> supply) will improve the nitrogen removal. One of these options is a complete nitrogen removal (ammonia to N<sub>2</sub>) by a mixed population of 'aerobic' ammonia oxidizers and anammox bacteria under anoxic conditions in the presents of NO<sub>2</sub> [101].

The interest in small treatment systems has often been overshadowed by concern over design, construction, and operation of large regional systems. Small systems were often designed as small-scale models of large plants. As

a consequence, many are operationally energy and resource intensive. New and innovative techniques like those described in the review might offer a solution for many treatment plants. The activated sludge process has been used extensively in its original form as well as in many modified forms. In the method used and the design of the process, consideration must be given to selection of the reactor type, loading criteria, sludge production, oxygen requirements and transfer, nutrient requirements, control of filamentous organisms, and effluent characteristics. More specific characteristics for the biological part are the operation factors like reaction kinetics, oxygen transfer, nature of the wastewater, local environmental conditions, construction, operation mode, and maintenance costs.

In view of these considerations, we believe there is no single best process for ammonium removal from wastewater. In each case it has to be evaluated which process is most suitable. Table 1 compares the different characteristics of new and established processes to allow a proper evaluation which method is best for a specific application.

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